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# FSFR-HS 系列 — 适用于半桥谐振转换器的先进的飞兆功率开关 (FPS™)

## 特性

- 为半桥谐振转换器拓扑提供了 50% 占空比的变频控制
- 通过零电压开关 (ZVS) 实现高效率
- 内置高侧栅极驱动器 IC
- 具有快速恢复类型体二极管 ( $t_{rr}=160$  ns 典型值) 的内部 UniFET™
- 为 MOSFET 优化的固定死区时间 (350 ns)
- 用于软启动高达 600 kHz 的工作频率
- 为所有保护提供自重启操作, 尽管具有外部  $V_{CC}$  偏压
- 具有可编程滞回的线电压 UVLO
- 通过线电压 UVLO 引脚实现简单的导通/关断
- 无需外部元件便可提供线电压 UVLO 与 FAN7930 兼容使用
- 保护功能 过压保护 (OVP)、过流保护 (OCP)、异常过流保护 (AOCP)、内部热关断 (TSD)

## 应用

- 等离子 (PDP) 与液晶 (LCD) 电视
- 台式计算机与服务器
- 适配器
- 通信电源

## 说明

FSFR-HS 是高度集成的电源开关, 专为高效率半桥谐振转换器而设计。它提供了构建可靠、强健的谐振转换器所需的一切, FSFR-HS 不仅简化了设计, 同时提高了生产力和性能。FSFR-HS 将功率 MOSFET 与高侧栅极驱动电路、精确的电流控制振荡器以及内置保护功能完美地整合在了一起。

高侧栅极驱动电路具有共模噪声消除功能, 它为稳定操作提供了出色的抗噪能力。使用零电压开关 (ZVS) 技术可显著降低开关损耗并提高效率。ZVS 还可以显著降低开关噪声, 即使工作频率增加也如此。除了高工作频率外, 它还提供少量的电磁干扰 (EMI) 滤波, 从而可缩小谐振腔, 并提高功率密度。

FSFR-HS 可用于谐振转换器拓扑, 如串联谐振、并联谐振以及 LLC 谐振转换器。

## 相关资源

[AN4151 — 使用 FSFR 系列飞兆电源开关 \(FPS™\) 的半桥 LLC 谐振转换器设计](#)

## 订购信息

器件编号	封装	工作结温	$R_{DS(ON\_MAX)}$	不带散热片的最大输出功率 ( $V_{IN}=350\sim400$ V) <sup>(1,2)</sup>	带散热片的最大输出功率 ( $V_{IN}=350\sim400$ V) <sup>(1,2)</sup>
FSFR1800HS	9-SIP	-40 至 +130°C	0.95 $\Omega$	120 W	260 W
FSFR1800HSL	9-SIP L-成型				
FSFR1700HS	9-SIP	-40 至 +130°C	1.25 $\Omega$	100 W	200 W
FSFR1700HSL	9-SIP L-成型				

### 注意:

1. 结温可限制最大输出功率。
2. 50°C 环境温度时开架式设计中的最大实际持续功率。

应用电路图

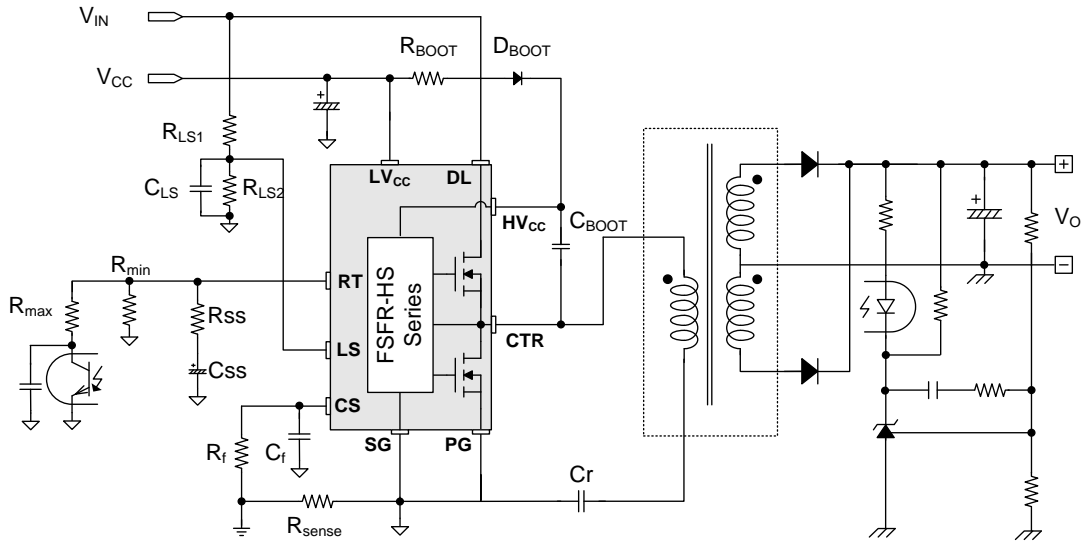


图 1. 典型应用电路 (LLC 谐振半桥转换器)

框图

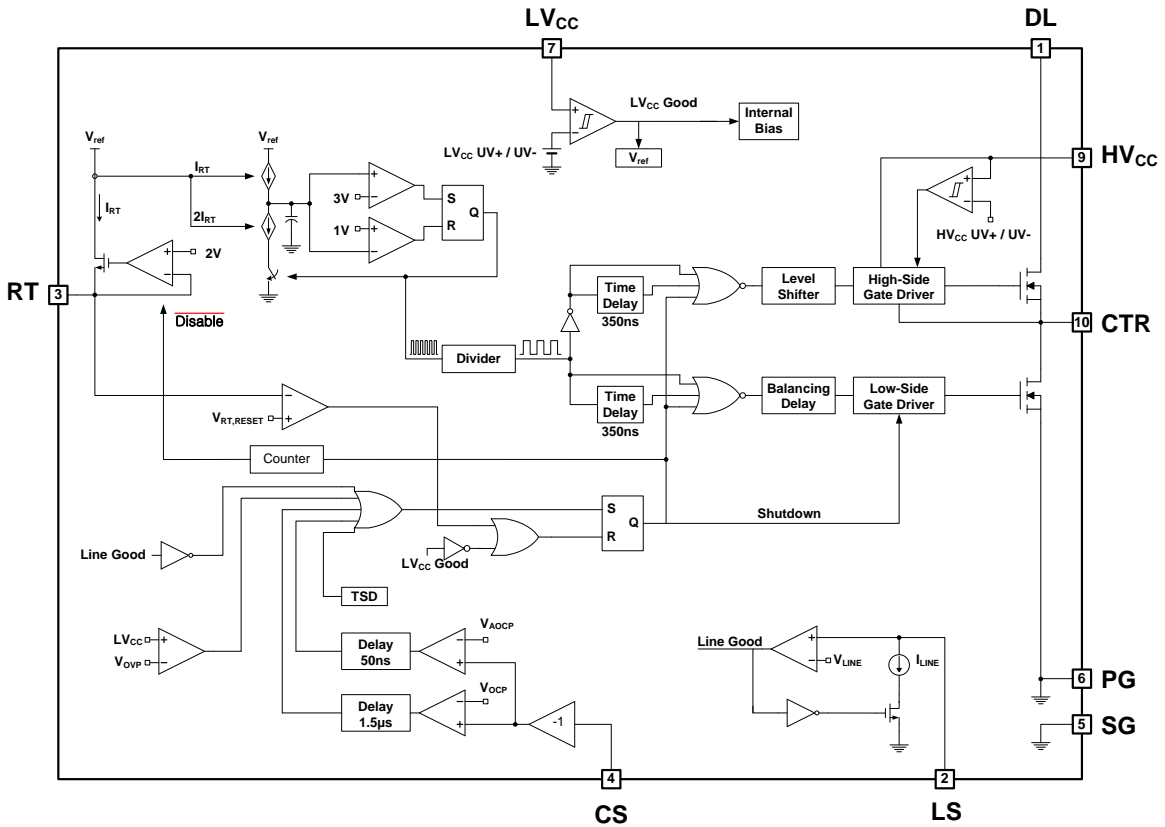


图 2. 内部框图

## 引脚布局

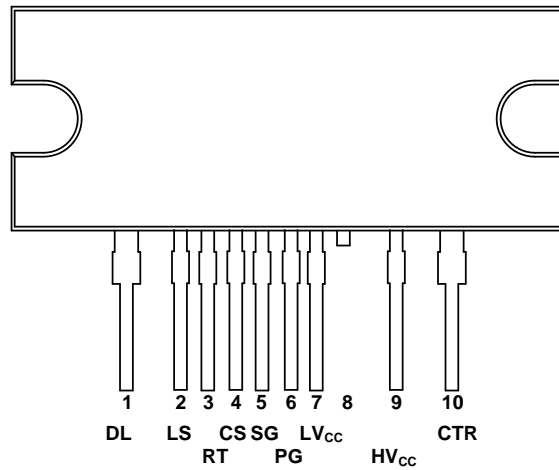


图 3. 封装图

## 引脚定义

引脚号	名称	说明
1	DL	这是高侧 MOSFET 的漏极，通常连接至高压直流输入。
2	LS	这是输入电压欠压锁定 (UVLO) 的线路感测引脚。
3	RT	此引脚用于控制正常操作下的开关频率。触发任何保护时，内部自动/重启 (A/R) 电路开始感测引脚上的电压，该引脚通过外部电阻自然放电。当电压减小 0.1 V 时，可通过 A/R 操作 IC。通常，连接光电耦合器控制用于输出电压调节的开关频率和用于设置最小/最大工作频率的电阻。
4	CS	此引脚检测流经低侧 MOSFET 的电流。通常，此引脚为负压。
5	SG	该引脚为控制部分的地。
6	PG	该引脚为电源地。该引脚连接到低侧 MOSFET 的源极。
7	LV <sub>CC</sub>	该引脚为控制 IC 的供电电压。
8	NC	无连接
9	HV <sub>CC</sub>	这是高侧栅极驱动电路的电源电压。
10	CTR	这是低侧 MOSFET 的漏极。典型地，变压器连接到该引脚。

## 绝对最大额定值

应力超过绝对最大额定值，可能会损坏器件。在超出推荐的工作条件的情况下，该器件可能无法正常工作，所以不建议让器件在这些条件下长期工作。此外，过度暴露在高于推荐的工作条件下，会影响器件的可靠性。绝对最大额定值仅是应力规格值。

符号	参数		最小值	最大值	单位
$V_{DS}$	最大漏极至源极电压 (DL-CTR 和 CTR-PG)		500		V
$LV_{CC}$	低侧电源电压		-0.3	25.0	V
HV <sub>CC</sub> 至 CTR	高侧 $V_{CC}$ 引脚至低侧漏极电压		-0.3	25.0	V
HV <sub>CC</sub>	高侧浮动电源电压		-0.3	525.0	V
$V_{RT}$	定时电阻连接和自动重启引脚电压		-0.3	5.0	V
$V_{LS}$	线电压感测输入电压		-0.3	$LV_{CC}$	V
$V_{CS}$	电流感测 (CS) 引脚输入电压		-5	1	V
$f_{sw}$	建议开关频率		10	600	kHz
$dV_{CTR}/dt$	允许的低侧 MOSFET 漏极电压压摆率			50	V/ns
$P_D$	总功耗 <sup>(4)</sup>	FSFR1800HS/L		11.7	W
		FSFR1700HS/L		11.6	
$T_J$	最大结温 <sup>(5)</sup>			+150	°C
	推荐的工作结温 <sup>(5)</sup>		-40	+130	
$T_{STG}$	存储温度范围		-55	+150	°C
<b>MOSFET 部分</b>					
$V_{DGR}$	漏极栅极电压 ( $R_{GS}=1\text{ M}\Omega$ )		500		V
$V_{GS}$	栅极源极 (GND) 电压			$\pm 30$	V
$I_{DM}$	脉冲漏电流 <sup>(6)</sup>	FSFR1800HS/L		23	A
		FSFR1700HS/L		20	
$I_D$	连续漏极电流	FSFR1800HS/L	$T_C=25^\circ\text{C}$	7.0	A
			$T_C=100^\circ\text{C}$	4.5	
		FSFR1700HS/L	$T_C=25^\circ\text{C}$	6.0	
			$T_C=100^\circ\text{C}$	3.9	
<b>封装部分</b>					
扭矩	建议螺栓扭矩		5~7		kgf·cm

### 注意：

- 这些参数尽管经过保证，也仅在 EDS（硅片测试）过程中测试。
- 每个 MOSFET（两个 MOSFET 都导通）。
- 所推荐的工作节温最大值受限于热保护功能。
- 脉冲宽度受限于最大结温。

## 热阻测试

除非另有规定，否则  $T_A=25^\circ\text{C}$ 。

符号	参数		数值	单位
$\theta_{JC}$	结壳中心热阻（两个 MOSFET 传导）	FSFR1800HS/L	10.7	°C/W
		FSFR1700HS/L	10.8	
$\theta_{JA}$	节-环境之间热阻		80	°C/W

## 电气特性

除非另有规定, 否则  $T_A=25^{\circ}\text{C}$ 、 $\text{LV}_{\text{CC}}$ 、 $\text{HV}_{\text{CC}}=17\text{ V}_{\text{DC}}$  和  $R_T=26\text{ k}\Omega$ 。

符号	参数	工作条件	最小值	典型值	最大值	单位
<b>MOSFET 部分</b>						
$\text{BV}_{\text{DSS}}$	漏极至源极击穿电压	$I_D=200\ \mu\text{A}$ , $T_A=25^{\circ}\text{C}$	500			V
		$I_D=200\ \mu\text{A}$ , $T_A=125^{\circ}\text{C}$		540		
$R_{\text{DS(ON)}}$	导通电阻	FSFR1800HS/L $V_{\text{GS}}=10\text{ V}$ , $I_D=3.0\text{ A}$		0.77	0.95	$\Omega$
		FSFR1700HS/L $V_{\text{GS}}=10\text{ V}$ , $I_D=2.0\text{ A}$		1.00	1.25	
$t_{\text{rr}}$	体二极管反向恢复时间 <sup>(7)</sup>	FSFR1800HS/L $V_{\text{GS}}=0\text{ V}$ , $I_{\text{DIODE}}=7.0\text{ A}$ , $di_{\text{DIODE}}/dt=100\text{ A}/\mu\text{s}$		160		ns
		FSFR1700HS/L $V_{\text{GS}}=0\text{ V}$ , $I_{\text{DIODE}}=6.0\text{ A}$ , $di_{\text{DIODE}}/dt=100\text{ A}/\mu\text{s}$		160		
$C_{\text{ISS}}$	输入电容 <sup>(7)</sup>	FSFR1800HS/L	$V_{\text{DS}}=25\text{ V}$ , $V_{\text{GS}}=0\text{ V}$ , $f=1.0\text{ MHz}$	639		$\mu\text{F}$
		FSFR1700HS/L		512		$\mu\text{F}$
$C_{\text{OSS}}$	输出电容 <sup>(7)</sup>	FSFR1800HS/L		82.1		$\mu\text{F}$
		FSFR1700HS/L		66.5		$\mu\text{F}$
<b>电源部分</b>						
$I_{\text{LK}}$	偏置漏电流	$\text{HV}_{\text{CC}}=V_{\text{CTR}}=500\text{ V}$			50	$\mu\text{A}$
$I_{\text{QHVCc}}$	$\text{HV}_{\text{CC}}$ 静态电源电流	$(\text{HV}_{\text{CC}}\text{UV}+) - 0.1\text{ V}$		50	120	$\mu\text{A}$
$I_{\text{QLVcC}}$	$\text{LV}_{\text{CC}}$ 静态电源电流	$(\text{LV}_{\text{CC}}\text{UV}+) - 0.1\text{ V}$		100	200	$\mu\text{A}$
$I_{\text{OHVCc}}$	工作 $\text{HV}_{\text{CC}}$ 电源电流 (RMS 值)	$f_{\text{OSC}}=50\text{ KHz}$		6	9	mA
		无开关		100	200	$\mu\text{A}$
$I_{\text{OLVcC}}$	工作 $\text{LV}_{\text{CC}}$ 电源电流 (RMS 值)	$f_{\text{OSC}}=50\text{ KHz}$		7	11	mA
		无开关		2	4	mA
<b>UVLO 部分</b>						
$\text{LV}_{\text{CC}}\text{UV}+$	$\text{LV}_{\text{CC}}$ 电源欠压正向阈值 ( $\text{LV}_{\text{CC,START}}$ )		11.2	12.5	13.8	V
$\text{LV}_{\text{CC}}\text{UV}-$	$\text{LV}_{\text{CC}}$ 电源欠压负向阈值 ( $\text{LV}_{\text{CC,STOP}}$ )		8.9	10.0	11.1	V
$\text{LV}_{\text{CC}}\text{UVH}$	$\text{LV}_{\text{CC}}$ 电源欠压滞回			2.5		V
$\text{HV}_{\text{CC}}\text{UV}+$	$\text{HV}_{\text{CC}}$ 电源欠压正向阈值 ( $\text{HV}_{\text{CC,START}}$ )		8.2	9.2	10.2	V
$\text{HV}_{\text{CC}}\text{UV}-$	$\text{HV}_{\text{CC}}$ 电源欠压负向阈值 ( $\text{HV}_{\text{CC,STOP}}$ )		7.8	8.7	9.6	V
$\text{HV}_{\text{CC}}\text{UVH}$	$\text{HV}_{\text{CC}}$ 电源欠压滞回			0.5		V
<b>振荡器与反馈部分</b>						
$V_{\text{RT}}$	RT 引脚上的输出电压	$R_T=26\text{ k}\Omega$	1.5	2.0	2.5	V
$f_{\text{OSC}}$	输出振荡频率		47	50	53	kHz
DC	输出占空比		48	50	52	%

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**电气特性(续)**除非另有规定, 否则  $T_A=25^{\circ}\text{C}$ 、 $LV_{CC}$ 、 $HV_{CC}=17\text{ V}_{DC}$  和  $R_T=26\text{ k}\Omega$ 。

符号	参数	工作条件	最小值	典型值	最大值	单位
<b>保护部分</b>						
$V_{RT,RESET}$	开始重启的阈值电压		0.07	0.12	0.17	V
$t_{DELAY,RESET}$	保护后禁用 OSC 电路的延迟	$f_{OSC}=50\text{ kHz}$		20		ms
$V_{LINE}$	输入电压的导通阈值		2.38	2.50	2.62	V
$I_{LINE}$	线电压 UVLO 的滞回电流		7.5	9.5	11.5	$\mu\text{A}$
$V_{OVP}$	$LV_{CC}$ 过压保护		21	23	25	V
$V_{AOCP}$	AOCP 阈值电压		-1.0	-0.9	-0.8	V
$t_{BAO}$	AOCP 消隐时间 <sup>(7)</sup>	$V_{CS} < V_{AOCP}$		50		ns
$V_{OCP}$	OCP 阈值电压		-0.64	-0.58	-0.52	V
$t_{BO}$	OCP 消隐时间 <sup>(7)</sup>	$V_{CS} < V_{OCP}$	1.0	1.5	2.0	$\mu\text{s}$
$t_{DA}$	延迟时间 (低侧) 从 $V_{AOCP}$ 检测到关断 <sup>(7)</sup>			250	400	ns
$T_{SD}$	热关闭温度 <sup>(7)</sup>		120	135	150	$^{\circ}\text{C}$
<b>死区时间控制部分</b>						
$D_T$	死区时间 <sup>(8)</sup>			350		ns

**注意:**

- 该参数由设计保证; 未经产品测试。
- 这些参数尽管经过保证, 也仅在 EDS (硅片测试) 过程中测试。

## 典型性能特征

这些特性图在  $T_A=25^\circ\text{C}$  标准化。

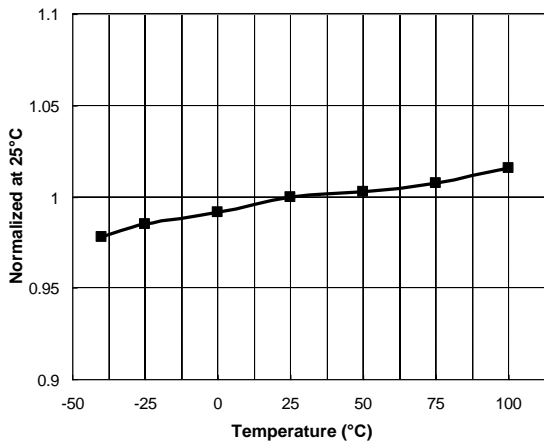


图 4. 低侧 MOSFET 占空比与温度的关系

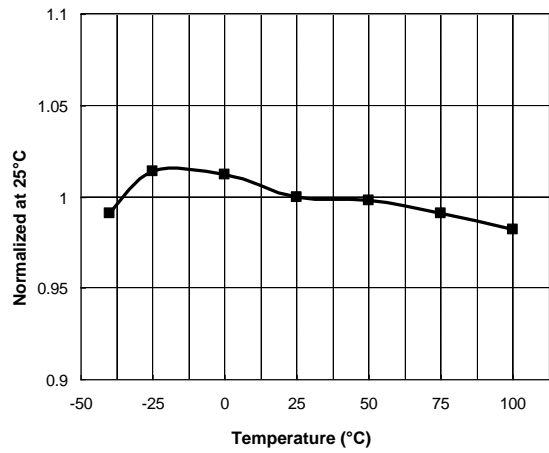


图 5. 开关频率与温度的关系

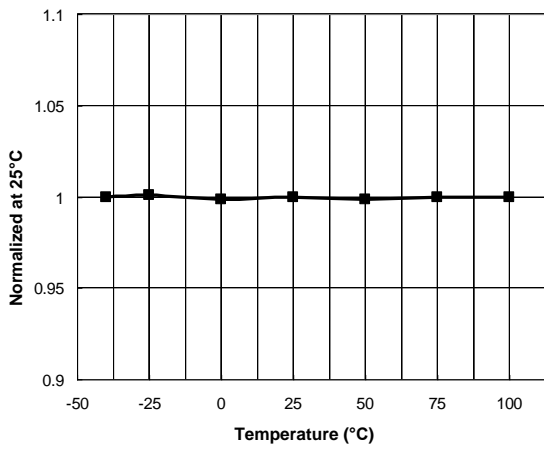


图 6. 高侧 V<sub>CC</sub> (HV<sub>CC</sub>) 启动与温度的关系

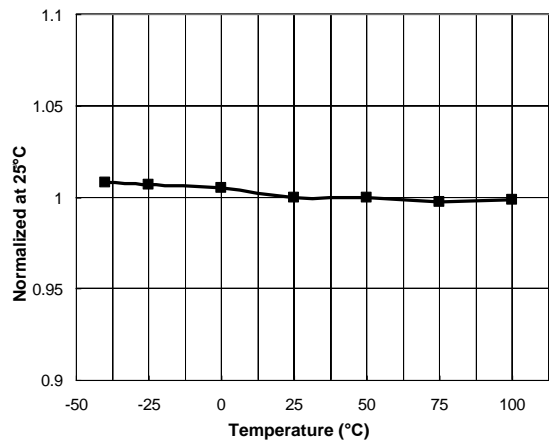


图 7. 高侧 V<sub>CC</sub> (HV<sub>CC</sub>) 停止与温度的关系

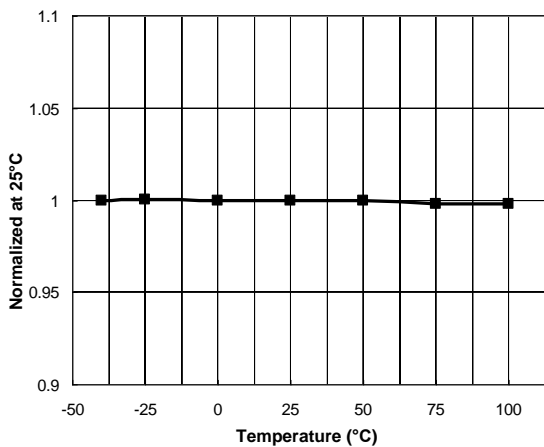


图 8. 低侧 V<sub>CC</sub> (LV<sub>CC</sub>) 启动与温度的关系

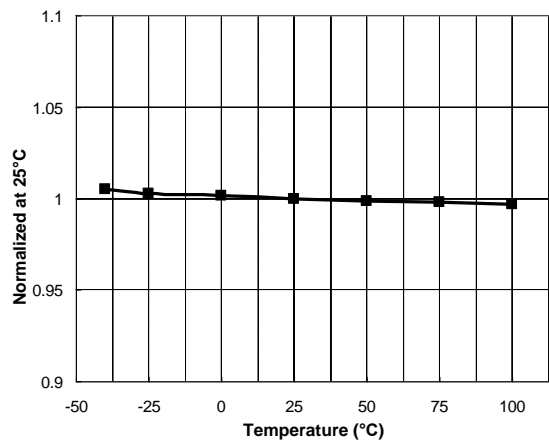


图 9. 低侧 V<sub>CC</sub> (LV<sub>CC</sub>) 停止与温度的关系



### 典型性能特征 (接上页)

这些特性图在  $T_A=25^\circ\text{C}$  下标准化。

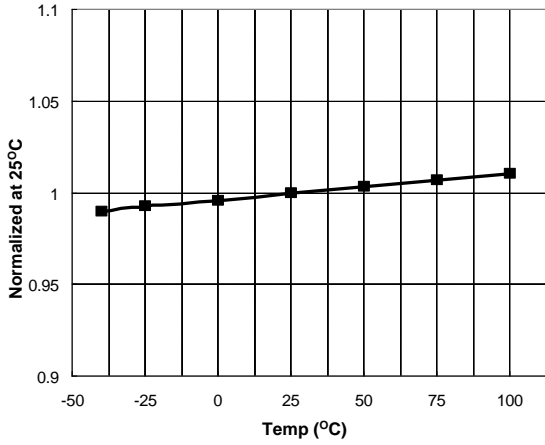


图 10. LV<sub>CC</sub> OVP 电压与温度的关系

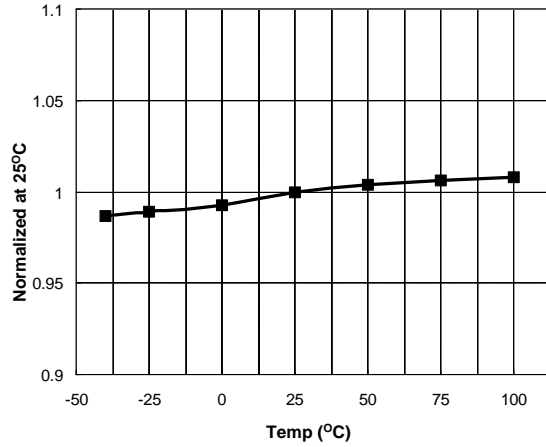


图 11. RT 电压与温度的关系

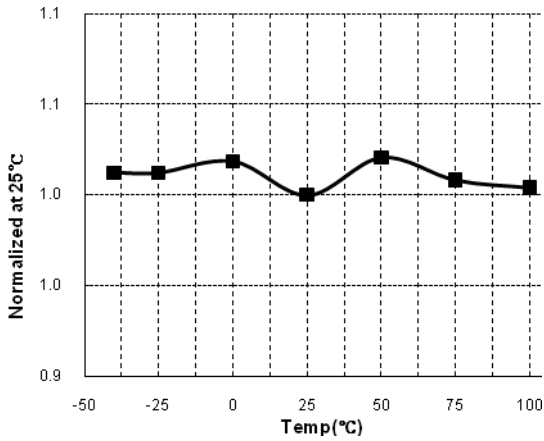


图 12. V<sub>RT,RESET</sub> 与温度的关系

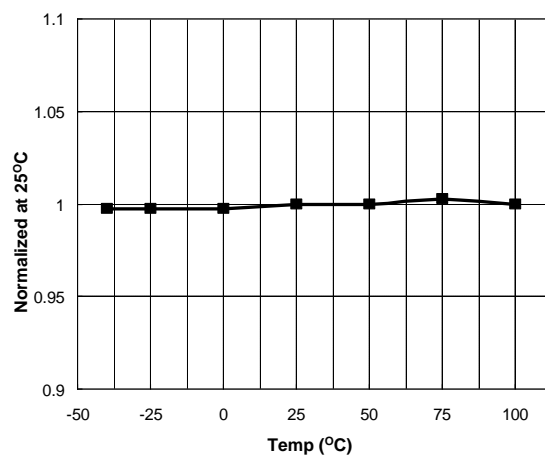


图 13. OCP 电压与温度的关系

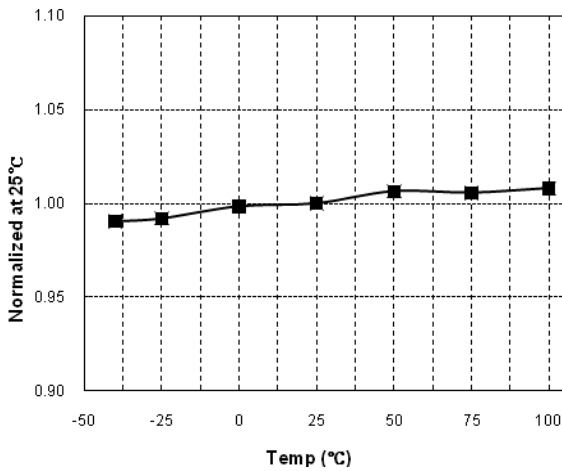


图 14. V<sub>LINE</sub> 与温度的关系

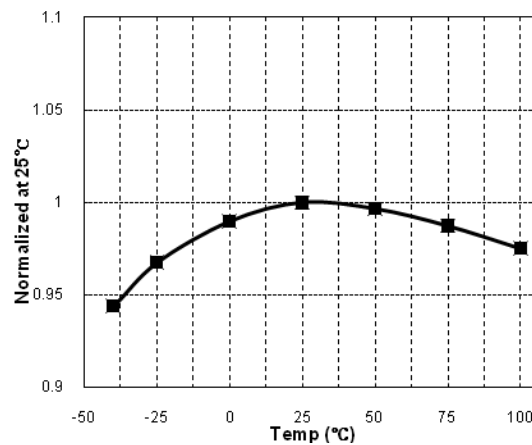


图 15. I<sub>LINE</sub> 与温度的关系

### 典型性能特征 (接上页)

这些特性图在  $T_A=25^\circ\text{C}$  下标准化。

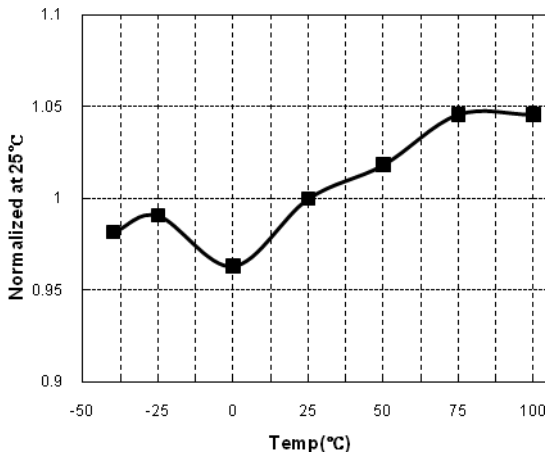


图 16.  $t_{\text{DELAY,RESET}}$  与温度的关系

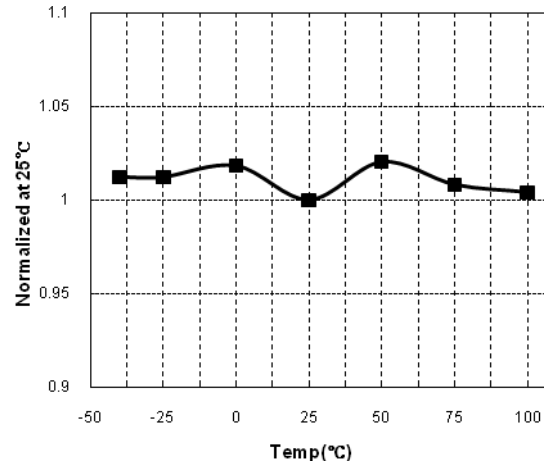


图 17.  $V_{\text{RT,RESET}}$  与温度的关系

## 功能说明

**1. 基本操作:** FSFR-HS 系列设计为驱动高侧和低侧 MOSFET，分别占 50% 占空比。在连续转换期间引入了固定死区时间 350 ns，如图 18 所示。

一旦  $LV_{CC}$  高于  $LV_{CC,START} = 12.5 V$ ，IC 即开始操作，生成低侧栅极信号并驱动低侧 MOSFET。自举二极管和电容由低侧 MOSFET 的工作期间得到电荷充电。在  $HV_{CC}$  上的电压增至达  $HV_{CC,START}$ （通常为  $9.2 V$ ）后，为 MOSFET 生成高侧栅极信号。

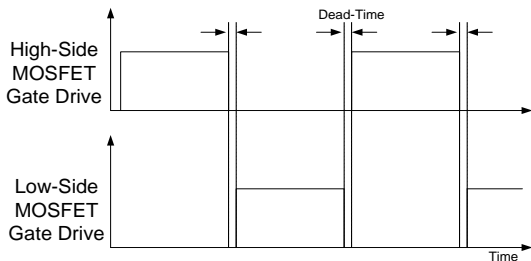


图 18. MOSFET 栅极驱动信号

**2. 内部振荡器:** FSFR-HS 系列采用电流控制振荡器，如图 19 所示。在内部，RT 引脚的电压调节在  $2 V$ ，并且振荡器电容  $C_T$  的充电/放电电流通过使用电流镜复制从 RT 引脚 ( $I_{CTC}$ ) 流出的电流来获得。因此，开关频率随着  $I_{CTC}$  的增加而增加。

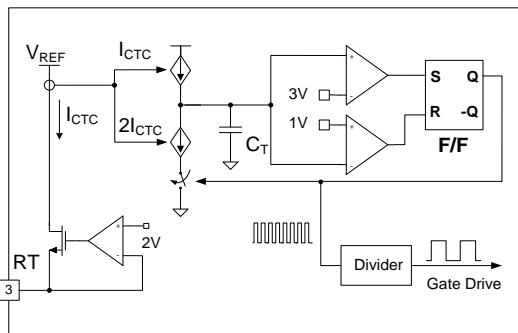


图 19. 电流控制的振荡器

**3. 频率设置:** 图 20 显示谐振转换器的典型电压增益曲线，其中增益与 ZVS 区中的开关频率成反比。输出电压可通过调制开关频率来调节。图 21 显示 RT 引脚的典型电路配置，其中光电耦合器电阻连接至 RT 引脚以调制开关频率。开关频率可从  $20 kHz$  控制到  $500 kHz$ 。

最小开关频率由下式确定：

$$f_{min} = \frac{1}{792p \times R_{min} + 0.54\mu} [Hz] \quad (1)$$

假定光电耦合器的饱和电压为  $0.2 V$ ，则最大开关频率由下式确定：

$$f_{max} = \frac{1}{792p \times R_{min} \parallel R_{max} + 0.54\mu} [Hz] \quad (2)$$

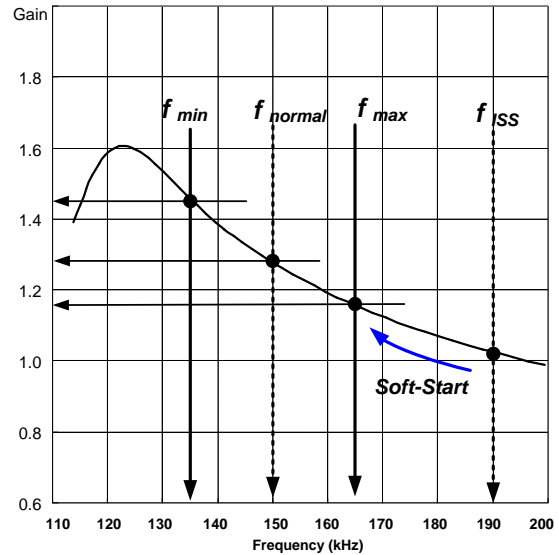


图 20. 谐振转换器典型增益曲线

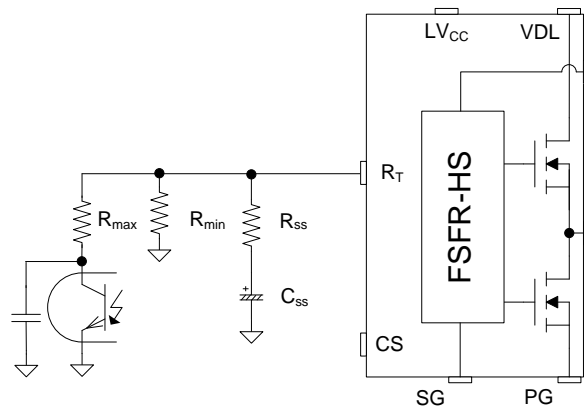


图 21. 频率控制电路

为避免过大的浪涌电流和启动时输出电压过冲，IC 需要逐渐增加谐振转换器的电压增益。由于谐振转换器的电压增益与开关频率成反比，因此实施软启动是通过从初始高频率 ( $f_{iss}$ ) 向下扫描开关频率，直至建立输出电压。

通过将 R-C 系列网络连接至 RT 引脚来建立软启动电路，如图 21 中所示。起初，工作频率由  $R_{ss}$  和  $R_{min}$  的并联阻抗设置。

初始最大频率可设置为高达 600 kHz，由下式确定：

$$f_{ss} = \frac{1}{792p \times R_{min} \parallel R_{SS} + 0.54\mu} [Hz] \quad (3)$$

软启动时间  $t_{SS}$ ，可由下式计算得出：

$$t_{SS} = 3 \times R_{SS} \cdot C_{SS} [s] \quad (4)$$

**4. 自动重启：**即使在有外部电源电压的情况下触发任何内置保护，FSFR-HS 系列也可自动重启。如图 22 和图 23 所示；一旦触发保护，功率 MOSFET 即停止。计数器开始操作并且对 1008 时钟进行计数，然后禁用 V-I 转换器。C<sub>SS</sub> 在通过电阻 R<sub>SS</sub> 和 R<sub>min</sub> 自然放电，直至 V<sub>RT</sub> 下降至 V<sub>RT,RESET</sub>，通常为 0.1 V。然后，复位所有保护并且 V-I 转换器恢复。FSFR-HS 再次通过软启动开始开关操作。

激活保护后的 1008 时钟的计数器工作时间由 RT 引脚流出的电流设定，直至 V<sub>RT</sub> 下降至 V<sub>RT,RESET</sub>。最后，可估算 FSFR-HS 的停止时间，不需考虑计数器工作时间，如：

$$t_{STOP} = 3C_{SS} \cdot (R_{SS} + R_{min}) [s] \quad (5)$$

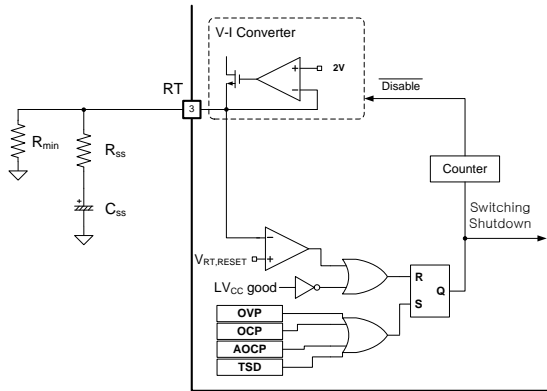


图 22. 自重启的内部框图

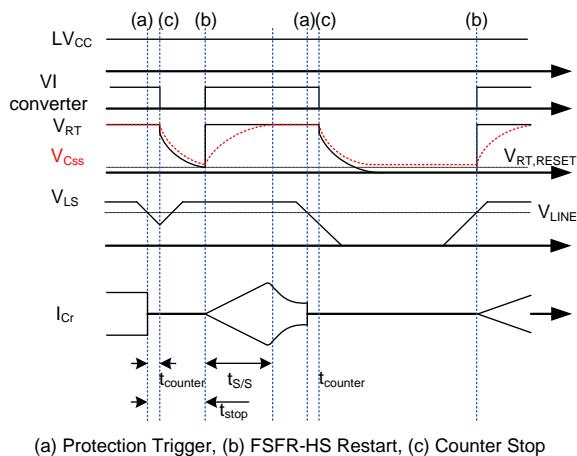


图 23. 自动重启操作

**5. 保护电路：**FSFR-HS 系列具有多个自我保护功能；如过流保护 (OLP)、异常过流保护 (OCP)、过压保护 (OVP)、热关断 (TSD) 和线电压欠压锁定 (LUVLO 或欠压)。这些保护为自动重启模式保护，如图 24 所示。

一旦检测到故障情况，开关操作即终止并且 MOSFET 保持关断。当 LV<sub>CC</sub> 下降至 10 V 的 LV<sub>CC</sub> 停止电压并且 V<sub>RT</sub> 低于 0.1 V 的 V<sub>RT,RESET</sub>，将复位保护。当 LV<sub>CC</sub> 达到 12.5 V 的启动电压时，FSFR-HS 恢复正常操作。

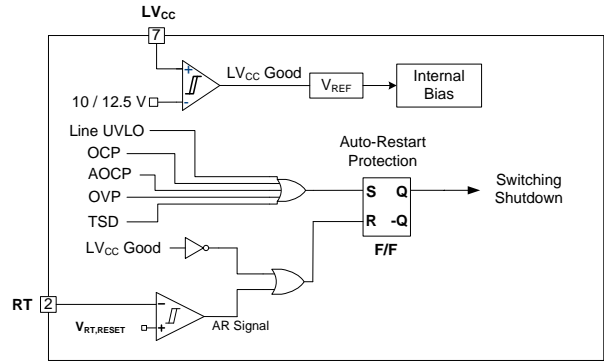


图 24. 保护框图

**5.1 过流保护 (OCP)：**当感测引脚电压降低至低于 -0.58 V 并且其持续时间超过 1.5 μs 的 OCP 消隐时间时，将触发 OCP 并且 MOSFET 保持关断。

**5.2 异常过流保护 (AOCPP)：**如果次级整流器二极管短路，具有极高 di/dt 的大电流可在触发 OCP 之前流经 MOSFET。如果感测引脚电压降低至低于 -0.9 V，将触发 AOCPP 且没有关断延迟。

**5.3 过压保护 (OVP)：**当 LV<sub>CC</sub> 达到 23 V 时，将触发 OVP。当变压器的辅助绕组向 FPS™ 供应 V<sub>CC</sub> 时，使用此保护。

**5.4 热关断 (TSD)：**MOSFET 和控制 IC 在一个封装中使控制 IC 检测 MOSFET 的异常过温变得更简单。如果温度超过约 130°C，将触发热关断。

**6. 线电压欠压锁定 (UVLO)：**FSFR-HS 包括具有可编程滞回电压的精密线电压 UVLO (或欠压)。当感测电阻 R1 和 R2 感测到的当直流母线电压变高时依直流母线电压成比例缩小的电压 V<sub>LS</sub> 高于 2.5 V 的 V<sub>LINE</sub> 时 (反之亦然)，此功能可启动或重启 IC。IC 启动和停止电压之间的滞回电压可由 I<sub>LINE</sub> 编程。在正常工作条件下，比较器的输出为高电平并且禁用 I<sub>LINE</sub>，因此 L<sub>S</sub> 引脚 V<sub>LS</sub> 上的电压可由 R1 和 R2 的分压获得。相反，当比较器的输出为低电平时，激活 I<sub>LINE</sub>。V<sub>LS</sub> 由流经 R1 的电流和 I<sub>LINE</sub> 的差异生成。

$C_{Filter}$  可用于减少变压器或开关转换引起的一些噪声。通常，几百 pF 至几十 nF 就够了，具体取决于噪声量。

启动与停止输入电压可以通过下式计算：

$$V_{dc-link,STOP} = V_{LINE} \times \frac{R1 + R2}{R2} [V] \quad (6)$$

$$V_{dc-link,START} = V_{dc-link,STOP} + I_{LINE} \times R1 [V] \quad (7)$$

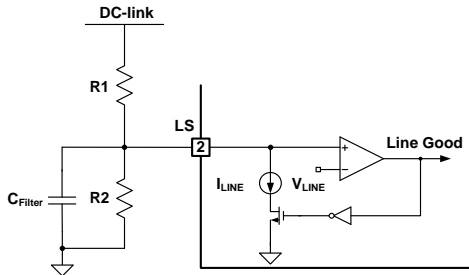


图 25. 半波检测

**7. 简单远程开关：**可使用可选自动重启模式关断功率级，如图 26 所示。

在自动重启模式下，为配置外部保护电路，需要采用了一个光电耦合器与 LS 引脚。当 LS 引脚上的电压下拉至低于  $V_{LINE}$  (2.5 V) 时，IC 在保持停止状态。但是，光电耦合器停止下拉时 IC 可自动执行自动重启操作。

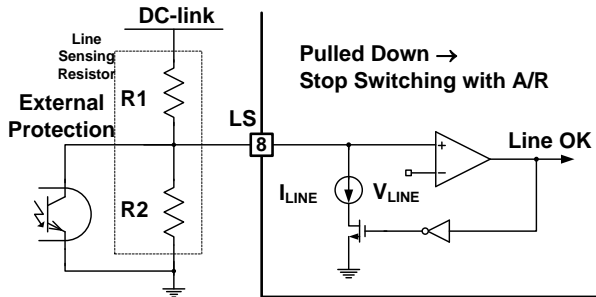


图 26. 外部保护电路

**8. 电流感测方法：**FSFR-HS 系列采用负压感测来检测 MOSFET 的漏极电流，这允许使用带小时间常数的滤波器的低噪声电阻感测和电容感测。

**8.1 电阻感测方法：**IC 可感测漏电流为负压，如图 27 和图 28 所示。半波感测允许感测电阻中较低的功耗，而全波感测在感测信号中具有较少的开关噪声。对于滤波器的时间常量范围， $3/100 \sim 1/10$  的工作频率是合理的。

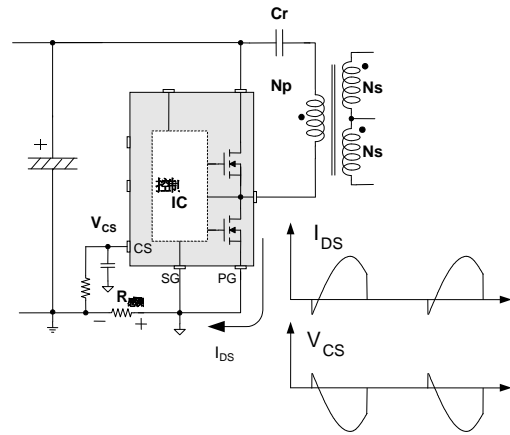


图 27. 半波检测

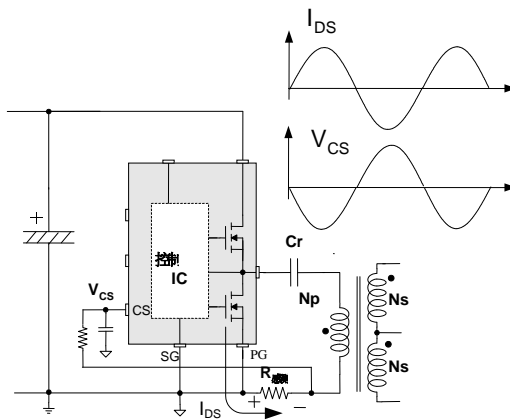


图 28. 全波检测

**8.2 电容感测方法：**漏极电流可以采用一个额外的与谐振电容并联的电容检测，如所示图 29。在低侧开关导通期间，通过  $C_B$  的电流  $i_{CB}$  使  $V_{SENSE}$  加在  $R_{SENSE}$  上。 $i_{CB}$  是  $i_p$  按阻抗比  $C_r$  和  $C_B$  的分流。一般地， $C_B$  与  $C_r$  比较合适的比值为  $1/100 \sim 1/1000$ 。 $R_D$  用作减少开关转换产生的噪声的阻尼。通常可使用数百欧姆至几千欧姆。

$V_{SENSE}$  可由下式估算得出；

$$V_{sense} = I_{Cr}^{pk} \frac{C_B}{C_r} \cdot R_{sense} [V] \quad (8)$$

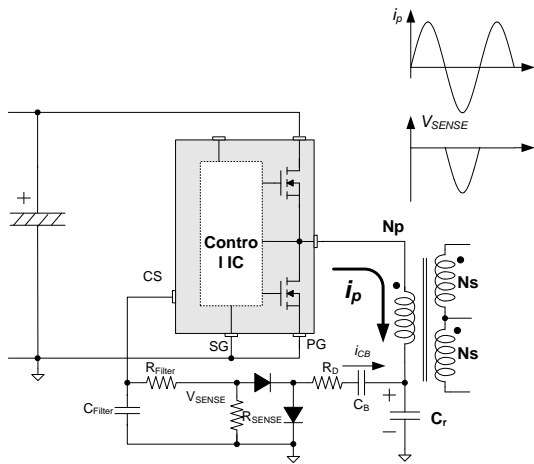


图 29. 电容检测

**9. PCB 布局指南:** 由于主变压器的辐射噪音、主变压器的次级端漏感不相等等原因可能发生占空比不平衡问题。RT 引脚附近的控制元件在 PCB 布局上被主初级端电流环路包围是造成占空比不平衡的主要原因。当高低侧 MOSFET 交替导通时，由初级端电流流向导致的元件上磁场的方向发生变化。方向相反的磁场产生通过、进入或从 RT 引脚流出的电流，这使得每个 MOSFET 的导通持续时间各不相同。强烈建议将 RT 引脚附近的控制元件与 PCB 布局上的初级端电流通路分开。图 30 显示占空比平衡情况的示例。

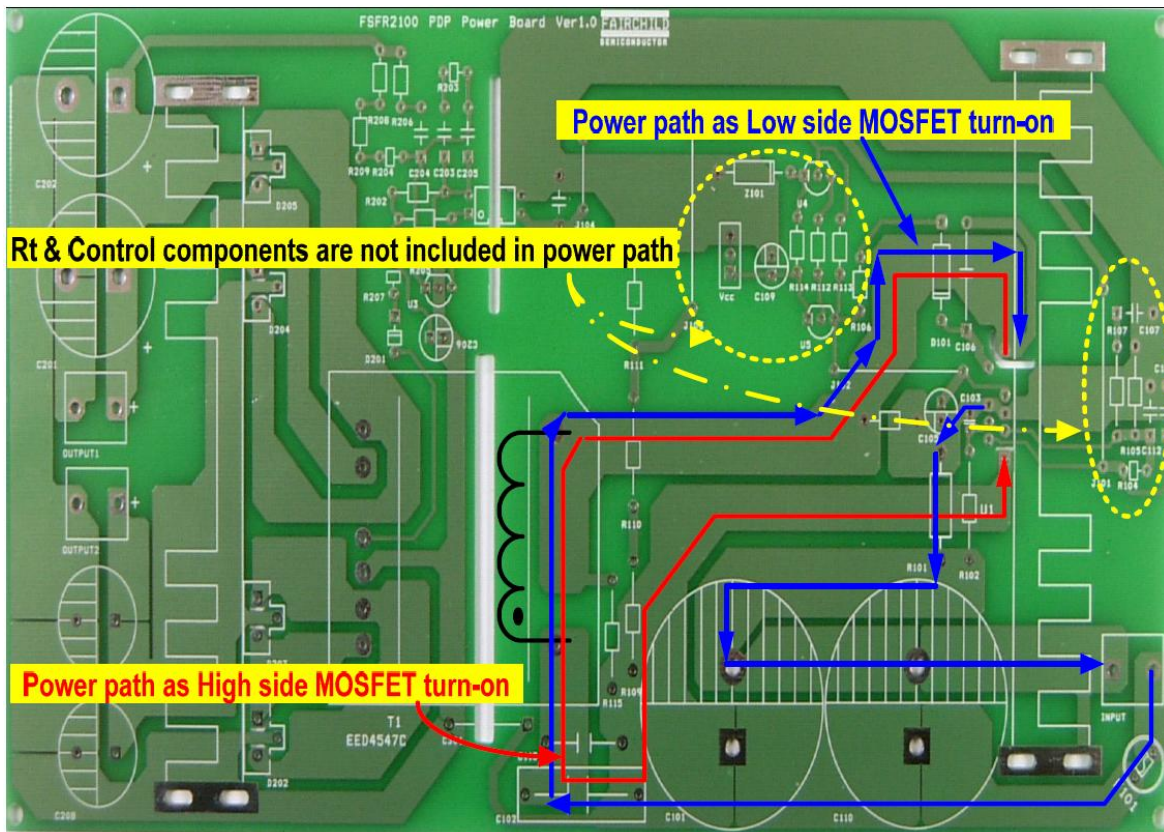
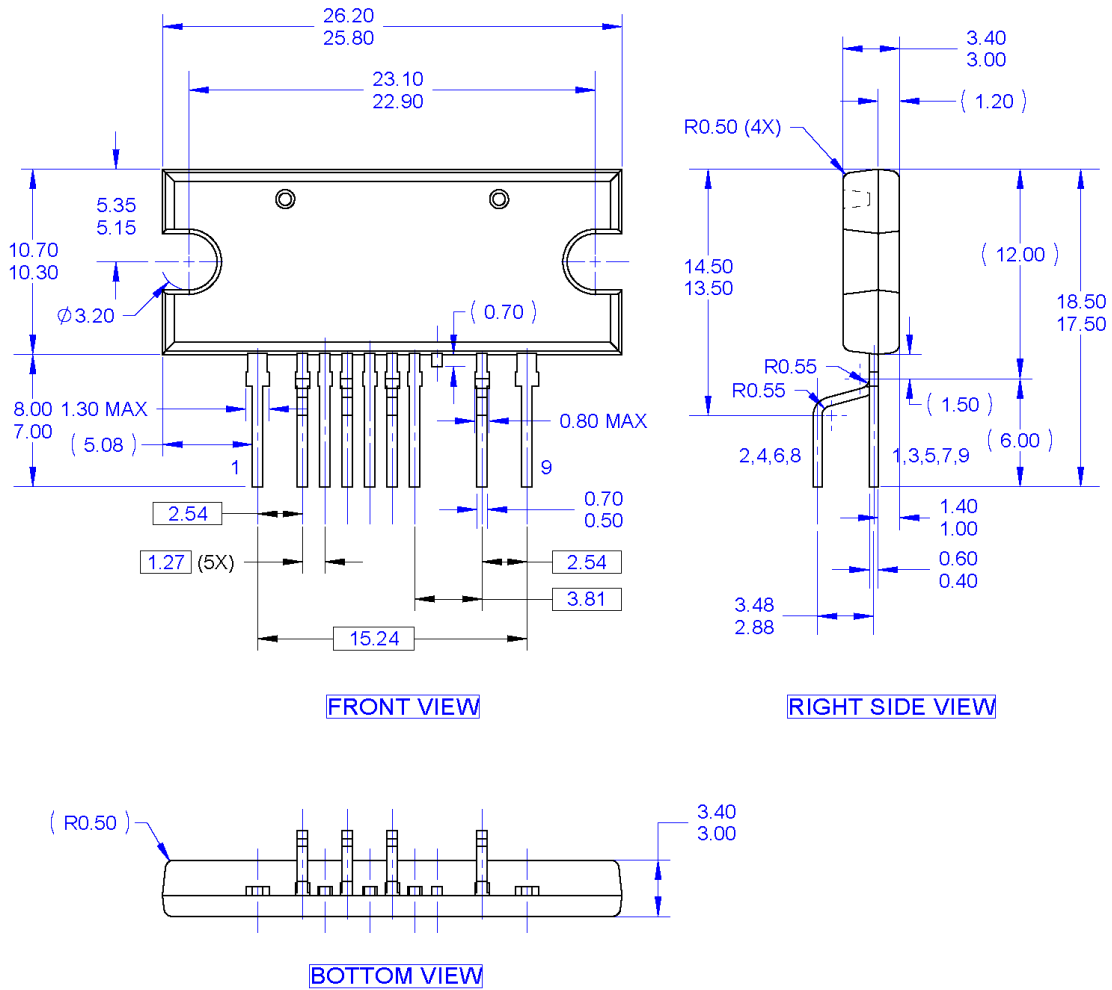


图 30. 占空比平衡的示例

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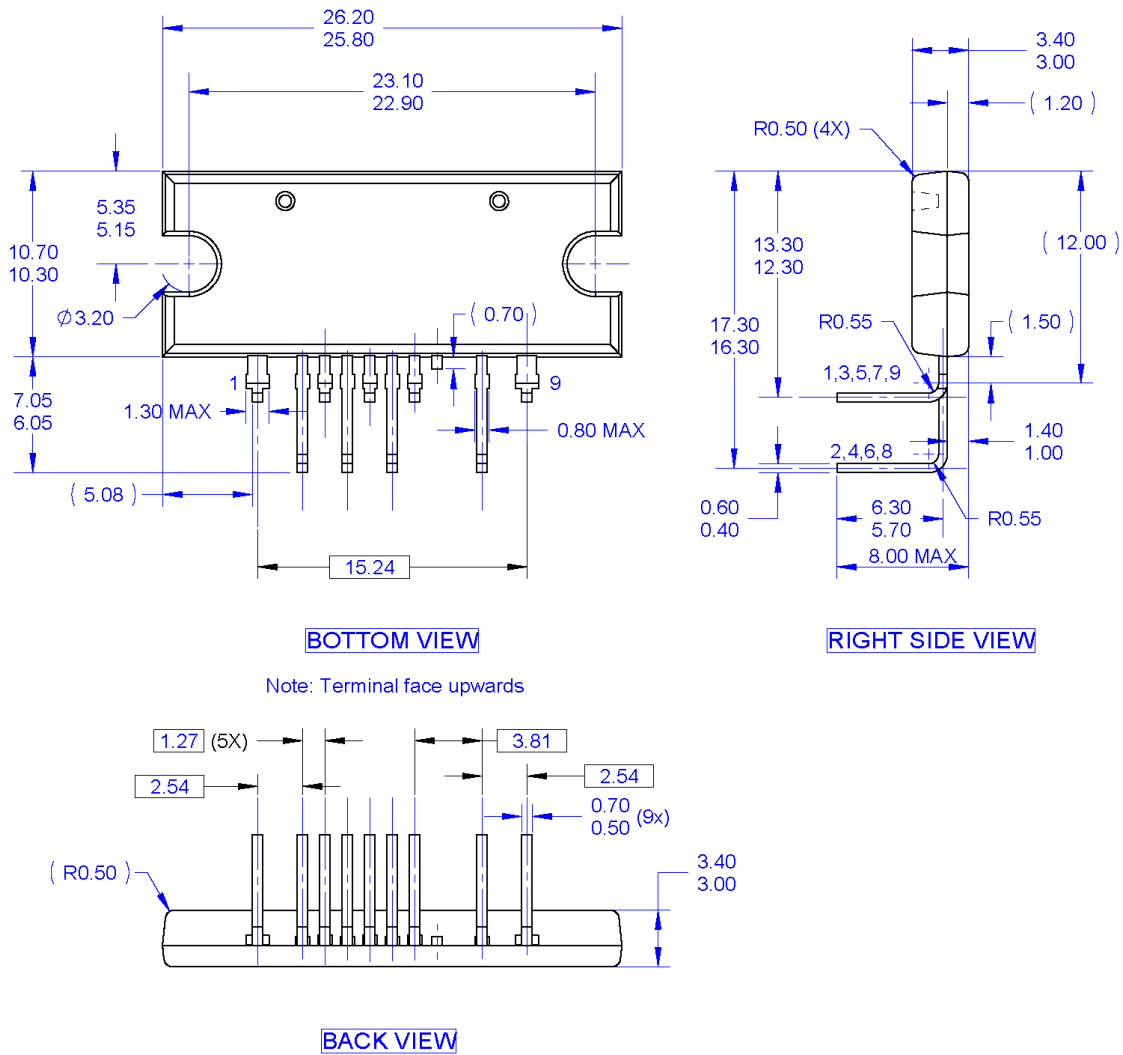
**图 31. 9 引脚、单线路内封装 (SIP)**

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**图 32. 9 引脚单线路内封装 (SIP) L 成型**

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